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A radiofrequency based sensor arrangement and a method

The invention relates to a sensor arrangement according to the preamble of claim 1.

In addition the invention relates to a method in conjunction with the sensor arrangement.

The leakproofness, low oxygen content and adequately low storage temperature of a package are the most important requirements for many packaged foodstuffs. When a protective gas package leaks, the protective gas travels out of the package, oxygen, damaging to the preservation of the quality of many products, gets into the package and the additional preservation provided by the original gas mixture of the package is lost. The passage of oxygen into the package is damaging also in the case of vacuum packages. In addition to the wholeness and storage temperature of a 15 package the high quality of a raw material used is an essential factor for maintaining organoleptic and microbiological quality particularly with uncooked products. As a result of the microbe activity occurring during the deterioration of a product, numerous amounts of evaporative compounds and compounds remaining in the product are generated whose quality and amounts are greatly affected by the nature and chemical composition of the foodstuff as well as by the microbe causing deterioration. These generated compounds affect on one hand the organoleptic quality of the foodstuff and on the other hand they function as indicators of microbiological quality of the foodstuff. The composition of the compounds generated by deterioration depends on the foodstuff, and for example in case of the deterioration of poultry the generation of different types of sulphur compounds (for example hydrogen sulphide, dimethyl sulphide, dimethyl disulphide) is typical.

Known applications associated with RF-reading techniques are for instance burglar 30 alarms and remote sensors (RFID).

The burglar alarms used in these applications are either destroyed or deactivated in a controlled manner. Remote sensors for their part are suitable only for recognition of a product or for saving a piece of information into the memory of a remote sensor. Burglar alarms and remote sensors do not have the ability to indicate cumulative events such as deterioration inside a foodstuff package.

The colour change of previously described indicators reacting to compounds generated in deterioration or to oxygen content of the package is visible. The primary function of visible indicators is to help the consumer evaluate the quality of the product at the time of purchase or at home. On the other hand on the part of wholesale and retail sales it would be efficient to verify the wholeness of the package and the quality of the product already before a consumer purchases it.

From WO 95/33991 is known a solution in which an indicator contains electronics and typically a screen that is integrated into the indicator. Alternatively, the indicator may have an output for sending a signal galvanically to the exterior measuring device. Such an indicator provided with its own screen is inevitably an expensive solution. Reading by an exterior device implemented by a galvanic connection is on the other hand quite an awkward way to obtain information from individual foodstuff packages.

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From e.g. US Patent 5,443,987, WO 9821120, EP patent 0666799 and WO 9904256 are known indicators in which a change in colour or outward appearance occurs when the product deteriorates.

From US patent 5,663,072 is known a solution in which by adding suitable chemi-20 cals the condition of a meat package can be evaluated by the changes of the absorption or reflective properties of the package itself upon exposure to electromagnetic radiation. The suitability of chemicals for use in foodstuffs may create problems and additionally the manner of measurement is quite inexact. 25

None of the hydrogen sulphide sensors described above is readable by RFtechniques nor are they suitable for placement in a foodstuff package and being read without breaking or touching the package. On the other hand the publications mentioned above also do not present application of RF-reading technology for measuring the quality of the packaged foodstuff.

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From application No. PCT/FI02/00911 is known a solution in which an indicator is placed inside a package, wherein the indicator is an LC (inductor-capacitor) circuit to which a sensor element is connected. The electrical properties of the sensor element change cumulatively as a result of deterioration of the product. The sensor reacts either directly to deterioration of the product or to evaporative compound resulting from deterioration or to oxygen gas that has leaked into the package. In this solution the sensor element is coupled by bonding or electricity-conducting glue

well suited for indicating the condition of perishable products such as foodstuffs or medicinal substances.

The basis of the invention is that the sensor element is coupled either through an alternate magnetic field (inductively) or through an alternate electric field (capacitively) to the reading device or the LC resonator.

More specifically, a sensor arrangement according to the invention is characterized by what is presented in the characterization part of claim 1.

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A method according to the invention is for its part characterized by what is presented in the characterization part of claim 12.

By using the invention, significant advantages are achieved.

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By using the solution according to the invention, the sensor elements can be manufactured at considerable less expense than using known art. Non-galvanic connection between the measuring circuit and the sensor enables a variety of technical implementations at reasonable expense, however, without compromising on the performance of the measurement. In solutions according to known art the forming of a galvanic contact to a very thin sensor film has been very difficult and sometimes nearly impossible and this problem the invention completely eliminates. When the sensor element is in practice a planar area, it is technically simple to manufacture.

The invention enables the manufacture of a single-use type of sensor very costeffectively.

In addition, the sensor is suitable for many different purposes of use.

- In the following the invention is described with the aid of embodiments according to the accompanying drawings.
 - Fig. 1 shows a perspective diagram of one inductively activated sensor arrangement according to the invention.

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- Fig. 2 shows the sensor element from the solution of Fig. 1.
- Fig. 3 shows a top view of another sensor structure according to the invention.

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- Fig. 4 shows a cross-sectional elevation view of the sensor structure as in Fig. 3.
- 5 Fig. 5 shows a top view of a third sensor structure according to the invention.
 - Fig. 6 shows a cross-sectional elevation view of a sensor structure as in Fig. 5.
- Fig. 7 a-c show as connection diagrams electrical equivalent circuits of an LC resonator suitable for the solution according to the invention.

1. Inductive coupling. The sensor element and metal ring inside the package.

In this embodiment of the invention, the element, being susceptible to measurable quantity, is disposed inside the package (not shown). The electrical conductivity or magnetic permeability of the element varies accumulatively in accordance to a measurable phenomenon. The electrical or magnetic properties of the element are measured outside the package inductively, wherein a deterioration event can be indicated reliably.

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The sensor element shown in Fig. 2 can be manufactured for example of silver or copper. The thickness of the planar metal layer is typically 30 nm, wherein for example already a small concentration of hydrogen sulphide (less than 1 microgram/litre) inside the package will cause within a few hours a relatively significant reduction in the average thickness of the element.

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According to Fig. 1 and 2, surrounding the sensor element 1 is a ring 2 made of metal. The metal of the ring, for example aluminium, is not susceptible to measurable gas or oxygen generated by deterioration. Essential in this embodiment of the invention is that the thickness of the metal ring 2 is significantly greater than the penetration depth into metal of the alternate magnetic field. For example, at a frequency of 8.2 MHz the penetration depth into aluminium is about 30 micrometers. The ring 2 must be significantly thicker than this, for example 100 micrometers. This means that the ring does not essentially reduce the Q-factor of the LC resonator. The size of the sensor element and the ring depends on from how great a distance it is desired for the reading device to be able to sense changes in the sensor element. For example, a reading distance of 2 cm requires that the outer diameter of the ring 2 is about 6 cm and the inner diameter about 5 cm, which is also the outer

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diameter of the disc-shaped sensor element. The ring 2 and sensor element 1 may also be round, oval, square or polygonal.

Inductive measurement is carried out such that a measuring coil 5 is placed outside the package such that it generates the alternate magnetic field 4 on the location of the element inside the package. The measuring coil 5 is tuned to resonance by coupling parallel to it a capacitance 3. The alternate magnetic field of the measuring coil 5 induces in the sensor element 1 and the metal ring 2 surrounding it an eddy current which for its part produces a magnetic field and induces a voltage in the measuring coil 5. The eddy currents induced in the sensor element 1 and the ring 2 are dependent upon their electrical conductivity, magnetic permeability and the thickness of their metal layers as well as the distance from the measuring coil to them. These eddy currents for their part induce in the measuring coil 5 a voltage which is then dependent upon all the aforementioned parameters. The frequency of the alternating current fed into the measuring coil 5 is changed such that the measurement occurs at resonance frequency and round about it. Resonance frequency can be, for example, in the range of 7.4 - 8.8 MHz, which is a license-free frequency area for inductive applications. From this measurement can be determined the resonance frequency of the measuring coil 5 and the quality factor of the resonance, the so-called Q-factor. The conductivity and thickness of the metal of the sensor element 1 is chosen such that due to the inductive coupling described above the sensor element 1 affects only the O-factor of the measuring coil. The Q-factor of the measuring coil is also dependent upon the distance between the sensor element and the coil. The ring around the sensor element is so thick that it affects the Q-factor only very slightly or essentially not at all. By contrast, due to inductive coupling, the closer it is, the more it decreases the effective inductance (L) of the measuring coil 5. The resonance frequency of the measuring coil can be calculated from the formula $f=1/(2\pi\sqrt{LC})$. Thus, the distance between the measuring coil 5 and the sensor element 1 can be determined from the measured changes in resonance frequency. When it is known, the Q-factor can be used to compensate for dependency on distance, after which the Q-factor indicates deterioration or the amount of oxygen in the package.

2. Inductive coupling. A sensor element for example within the LC resonator inside the package.

In a second embodiment of the invention, the sensor element is a part of the LC resonator such that it couples inductively (by an alternate magnetic field) to the LC

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resonator. This alternative is shown in Fig. 3 and 4. The sensor element 1 and the LC resonator 3, 5 form a transponder, which is disposed inside the package. This complex is formed from the base 6 which is of same insulating material, wherein the one of the electrodes 7 of the capacitor 3 is on the other side of the base 6 and the other electrode 7 of the capacitor 3 is formed by a part of the coil 5 on the opposite side of the base 6. The transponder means in this case an independent component that is capable of receiving and sending signals at radio frequencies. The planar sensor element 1 is formed in the centre of the coil 5 on the opposite side of the substrate 6 in relation to the coil 5. The sensor element 1 can, of course, also be with the coil 5 on the same side. Measurement is carried out otherwise similarly as in the embodiment of Fig. 1 and 2, but the reader (not shown) located outside the package couples inductively by an alternate magnetic field to the LC resonator 3, 5, The reader measures the Q-factor and the resonance frequency of the LC resonator located inside the package as shown in the embodiment of Fig. 1 and 2. The Ofactor of the LC resonator is dependent upon deterioration of the product or the amount of oxygen in the package. In this case the result of measurement is independent on the distance between the reader and the sensor element. The O-factor measured is directly proportional to deterioration of the product or the amount of oxygen in the package.

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3. Capacitive coupling. A sensor element within the LC resonator inside the package.

A third embodiment of the invention is similar to the second embodiment. In the third embodiment shown in Fig. 5 and 6, the coupling between the sensor element 1 and the LC resonator 3 and 5 is however capacitive. It can be implemented for example such that a planar sensor element 1 is disposed in the electric field induced by the wires of a multi-turned coil 5, in practise, on top of the insulating plate 8 arranged above the coil 5. As in the second embodiment, the measured Q-factor is directly proportional to deterioration of the product or the amount of oxygen in the package.

A sensor arrangement according to the invention as described in the above embodiments can be, for example, one of the following combinations:

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a) A combination of LC resonator 3 and 5 contained in the reader for a separate sensor 1 and its bordering ring 2 (example 1).

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- b) A combination of sensor 1 and transponder (coil and capacitor) (examples 2 and 3) in which the sensor element 1 and the LC resonator are of the same mechanical complex.
- According to Fig. 7a, an LC resonator is with ideal components a pure parallel coupling of a coil 5 and a capacitor. In this case a sensor element according to the invention inductively or capacitively affects the properties of either the coil 5 or the capacitor 3.
- According to Fig. 7b, in the equivalent circuit suitable for the invention a serial resistor R1 can be used between the coil 5 and the poles of the capacitor 3. Some LC resonators R1 of known art have had an element susceptible to changes. The resistor R1 can then be a real component or it can represent an imperfection of the coil 5, a resistive component. In this alternative, as well, a sensor element according to the invention inductively or capacitively affects the properties of either the coil 5 or the capacitor 3.

In Fig. 7c is shown, in addition to the components of Fig. 7b, a resistor R2 coupled in parallel with the capacitor 3, wherein the resistor can be a real component or alternatively it can represent an imperfection of the capacitor. In this alternative, as well, a sensor element according to the invention inductively or capacitively affects the properties of either the coil 5 or the capacitor 3.

In place of a cumulative sensor, other types of resistance-containing sensors can also be used. For example, the sensor can indicate a peak value, wherein an irreversible non-cumulative sensor element is used. Alternatively, the sensor can indicate a momentary value, wherein a reversible sensor element is used.

Also non-linear sensors, such as logarithmically or exponentially reacting sensors are in the scope of the invention entirely possible applications.

Also indexing sensors are suitable for the basic idea of the invention. These types of sensors are particularly practical in the case that it is desired to indicate the exceeding of a particular limit value.

In addition to different gases, the sensor element 1 can indicate e.g. moisture (water in different states or relative humidity), fluids, temperature, electromagnetic radiation or, for example, pressure.

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According to the invention, a sensor element is coupled to the LC resonator in terms of circuit technology only capacitively or inductively without a galvanic contact. Inside the package there may be a high-resistive connection through the contents of the package between the sensor and the LC resonator, but in terms of measuring technology this is insignificant. In the scope of the invention a capacitative or inductive coupling means then that in terms of circuit technology the LC resonator and the sensor are not galvanically in contact.

In place of a cumulative sensor element, a sensor element showing a peak value may be used, which is reversible. Also non-linear sensor elements, such as logarithmically or exponentially reacting sensors are in the scope of the invention entirely possible applications. Also indexing sensors are suitable for the basic idea of the invention.

In the sensor or transponder structure itself can, of course, be included a microchip performing other functions.

A solution according to the invention can also be further improved for example by adding layers to protect or strengthen the sensor element or the transponder, sticking glue can be added to it for attaching, it can be laminated directly to the package or to different types of structures or it can be a discrete sensor. In addition, a sensor element or transponder according to the invention can also be implemented by many more solutions than has been shown in the examples.